The recent advancements in GaN-based laser diodes by Nakamura et al. \(^1\) were achieved in part due to the use of the lateral epitaxial overgrowth (LEO) technique reported earlier for GaN films by several investigators using sapphire \(^2\)–\(^5\) and on 6H–SiC \(^6\)–\(^11\) substrates. Transmission electron microscopy (TEM) studies have been conducted by Zheleva et al. \(^8\),\(^10\),\(^11\) on GaN pyramids and stripes selectively grown from circular openings and rectangular windows, respectively, contained within SiO\(_2\) masks deposited on GaN/AlN/6H–SiC(0001) heterostructures. This research revealed that the volumes of the pyramids and stripes which laterally overgrew the masks contained \(<10^4–10^5\) dislocations/cm\(^2\). This was in contrast to the regions of vertical growth within the SiO\(_2\) windows which exhibited a density of threading dislocations of \(10^9–10^{10}\) cm\(^{-2}\). The crystallographic templates for lateral epitaxy of GaN are the \{11\20\} side facets when the SiO\(_2\) stripes are oriented along \{1\1\00\}, and the \{1\1\00\} and \{1\0\1\} side GaN planes if the stripe windows are oriented along \{1\1\20\} direction. The vertical growth direction in both cases is \{0001\}.

Stress/strain fields in a heterostructure consisting of LEO GaN deposited within two striped windows in a SiO\(_2\) mask, the latter deposited on a GaN/AlN/6H–SiC(0001) substrate, were modeled using two-dimensional (2D) finite element analysis (FEA), in-plane strain conditions and the code ANSYS 5.3.\(^12\) Two units of the heterostructure being analyzed were discretized using a quadratic four node element. The heterostructure was modeled within the framework of the continuum linear elasticity theory (Hook’s law is valid, and hence the stress and strain tensors are linearly related via the elasticity tensor). The boundary conditions were such that all nodes on the side faces of the model were fixed against displacements in the respective directions of the surface normal. The nodes on the bottom of the 6H–SiC substrate were fixed against displacements in the z direction to avoid rigid body shift. Elastic constants, Poisson’s constants, coefficients of thermal expansion, density and the temperatures of the initial and final state were used as input parameters.\(^13\)–\(^15\) The thermal load was applied considering the mismatches in thermal expansion coefficients without taking into account the lattice mismatches among the phases in the heterostructure. Room temperature was chosen as the reference temperature and the growth temperature for the LEO GaN (1100 °C) was chosen for the thermal load temperature. Various geometrical factors played important roles regarding the final thermal stress/strain field distribution and hence the final deformed shape in the heterostructure: (i) the width and the thickness of the GaN stripes, (ii) the openings in the SiO\(_2\) windows, (iii) the SiO\(_2\) film thickness, (iv) the thickness of the underlying GaN, and (v) the thickness of the AlN. In this study, the variation of the thermal stress as a function of the lateral growth distance, i.e., the width of the GaN stripes at a fixed window size was considered. A 2D, static model was employed. Though simple, this model described closely the morphology of the LEO GaN structures repeatedly observed by TEM.

A typical cross-sectional TEM image of a GaN stripe is shown in Fig. 1. As noted above, the density of threading dislocations is four to five orders of magnitude lower in the
laterally overgrown regions compared to that in the GaN material within the SiO₂ window. The airfoil shape of the LEO GaN, pointed to by the arrow in Fig. 1, formed in response either to the thermal stresses generated on heating prior to deposition of the LEO GaN and due to the differences in the coefficients of thermal expansion of the underlying GaN and SiO₂, or after the vertical growth of the GaN from the SiO₂ windows, followed by lateral overgrowth. Some of the observed coalesced regions contain voids of different shape including drop-like, key-hole-like or triangular, as shown in Fig. 2. If the LEO GaN film is sufficiently thick, these voids terminate within this volume of the film. Above the voids, the volume of coalescence is usually without observable dislocations.

The stress-distribution results from the FE calculations are shown in Figs. 3(a)–3(c) and based on the assumption of heating the complex LEO structure from room temperature to 1100 °C. The minimum stress (maximum stress relaxation) in each of the GaN stripes is along the boundary between the tensile and compressive fields. The cross-sectional shape of the GaN stripe follows approximately the variation in the stress fields, i.e., the profiles in the stress gradients. It is known that the stresses in a heterostructure can be accommodated by two mechanisms: mechanical deformation and/or defect generation and propagation. It is evident from the FE analysis that stresses are generated as a result of the mismatch in the coefficients of thermal expansion among the phases in these heterostructures, which cause bending in the areas of lateral epitaxy, as shown in Figs. 1 and 2(a). The observed shape of these deformed areas and the corresponding thermally generated stress/strain profiles determined by FE analysis resemble the morphologies observed for many laterally grown GaN structures. Characteristics of the temperature-dependent stress profiles include: (i) localization of the ~3 GPa maximum compressive stress at the corners of the GaN stripes along the x direction corresponding to the interface line along the (1120) direction; (ii) smaller localized compressive stress fields of ~1.5 GPa at the corners of the GaN stripes along the [0001] direction, or the vertical with respect to the interface planes, and (iii) localized shear stresses of ~0.9 GPa at the LEO GaN edges [Fig. 3(c)]. These stresses in tandem with the tensile stress of ~0.3 GPa along the side edges of the LEO GaN cause the deformation observed at the side faces of the GaN stripes. This deformation determines the formation and shape of the voids in the regions of coalescence.
Compressive and tensile stresses occur along the $x$ and $y$ directions in the LEO GaN adjacent to the SiO$_2$ windows as shown in Figs. 3a and 3b, respectively. These stresses are believed to cause the airfoil shape in the SiO$_2$ and the commonly observed fracture in the LEO GaN either near the window areas at the GaN/SiO$_2$ interfaces or within the SiO$_2$. An increase in the lateral dimension of the LEO region tends to reduce slightly the thermally generated compressive stresses along the GaN/SiO$_2$ interface line ($x$ direction) and increase the compressive stresses along the (0001) direction, as shown in Fig. 4.

Analysis of the shear stress is also important, since the localization of the maximum in this stress likely represents the sites for the onset of plastic relaxation, i.e., dislocations nucleation and propagation and/or film separation. The data presented in Fig. 4 indicate that an increase in the lateral epitaxy region also leads to an increase in the localized maximum shear stresses at the corners of the LEO GaN/SiO$_2$ interface. Thus, two keys to achieving defect-free GaN are: (i) control of the lateral epitaxy and (ii) knowledge regarding the variations in the thermal stress fields in this type of heterostructure.

In summary, TEM studies of selectively and laterally grown GaN stripes have revealed an airfoil-like morphology of the SiO$_2$ mask layer and void formation within the LEO GaN layers. FEA of these heterostructures indicated deformation, the deformed shapes likely to be observed and the distribution of the critical stresses. Employment of FEA for the analysis of the stress–strain fields distributions and the corresponding stress gradients within the LEO structure can be utilized to predict and optimize the necessary geometric conditions and the exact geometrical parameters ratios that will result in a structure with the required characteristics in crystal morphology.

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