

# Channel Walls Interaction Through the Liquid

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## I. INTRODUCTION

**1.1. Subject.** The problem discussed is a part of more large investigation on dynamical behaviour of water-filled cavities with a special geometry and bounded partially by elastic walls. Such cavities are broadly used as structural components in the buildings of the classical (hydraulic) power stations; in nuclear reactor technologies (as tanks and different basins (e.g. for pressure suppression, etc.)); in chemical industry and biotechnologies (as reactors, brawing chambers, etc.); in architecture as usual premises with window plates (or door plates, etc.); in ship structures, etc.

**1.2. Physical description.** In a thinwalled channel with a rectangular cross section inviscid, compressible and heavy liquid is flowing with a velocity on an infinity  $V \ll c$ , where  $c$  is its sound velocity. Two of the channel walls are infinitely rigid, other pair of them being characterized by a finite given rigidities  $EI_1$  &  $EI_2$ , correspondingly. All geometrical dimensions of the cross section are given, Fig. 1. The channel is infinitely long and the whole problem does not depend on the longitudinal co-ordinate. So the problem is planar one.

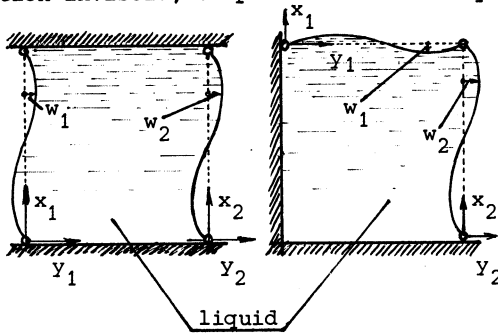


Fig. 1. Two schemes of the channel wall interaction.

For the first scheme  $w_1 = w_1(x, t)$  and  $w_2 = w_2(x, t)$  are displacement functions and for the second scheme  $w_1 = w_1(y, t)$  and  $w_2 = w_2(x, t)$ . All demonstration will be provided following No 1 scheme.

**1.3. Analytical description of the problem.** It is supposed that the "hydroelastic" mechanical system "two plates + liquid" is in state of free vibration with small amplitudes of  $w_1$  and  $w_2$  generating into liquid small acoustical perturbations. The displacement functions  $w_1(x, t)$  &  $w_2(x, t)$  have to satisfy the boundary problem:

$$(1) \quad (EI)_1 w_1^{IV} + \bar{m}_1 \ddot{w}_1 = -p_a - p_g, \quad (EI)_2 w_2^{IV} + \bar{m}_2 \ddot{w}_2 = +p_a + p_g;$$

$$(2) \quad x = 0, L: \quad w_1 = 0, \quad w_1'' = 0, \quad w_2 = 0, \quad w_2'' = 0,$$

where  $\bar{m}_1$  &  $\bar{m}_2$  - masses per  $1m^2$  of the walls vibrated;  $p_a$  - acoustical pressure;  $p_g$  - gravitational (statical) pressure;  $(-)^{IV} = (\partial^4/\partial x^4)$ ;  $(\dot{\phantom{x}}) = (\partial/\partial t)$ .

Further, the liquid motion is supposed to be potential one with velocity potential function  $\Psi = \Psi(x, y; t)$  which has to satisfy the boundary problem:

$$(3) \quad \Delta\varphi - (1/c^2) \cdot (\partial^2\varphi/\partial t^2) = 0, \quad \Delta = (\partial^2/\partial x^2) + (\partial^2/\partial y^2);$$

$$(4) \quad \begin{array}{ll} x = 0 & (\partial\varphi/\partial x) = 0; \\ x = h & (\partial\varphi/\partial x) = 0; \end{array} \quad \begin{array}{ll} y = 0 & (\partial\varphi/\partial y) = (\partial w_1/\partial t), \\ y = L & (\partial\varphi/\partial y) = (\partial w_2/\partial t). \end{array}$$

If the velocity potential is known,

$$(5) \quad \vec{v} = \text{grad}\varphi, \quad p_a = -\rho \cdot (\partial\varphi/\partial t).$$

As the gravitation pressure (including preliminary inner pressure  $p_0$ )

$p_g = -p_0 - \rho \cdot g \cdot (h-x)$  is known, we shall not consider it further.

## II. ANALYTICAL SOLUTION

2.1. Local co-ordinates. To be able to treat the problems of both geometrical schemes (Fig. 1) local co-ordinate systems  $(0, x, y_1)$  and  $(0, x, y_2)$  are introduced. They are connected by the formulas

$$(6) \quad x_1 \equiv x_2 \equiv x; \quad y_1 = L + y_2, \quad z_1 \equiv z_2 \equiv z.$$

2.2. Local potential functions. Let us introduce so called local denotations of a velocity potential function

$$(7) \quad \varphi_I = \varphi_1 + \varphi_{2(2 \rightarrow 1)}, \quad \varphi_{II} = \varphi_{1(1 \rightarrow 2)} + \varphi_2$$

which have to be read: "The velocity potential of all liquid motion in near vicinity of plate No 1 is equal to the sum of the "own" velocity potential function  $\varphi_1$  describing the liquid motion generated by No 1 plate vibrations and velocity potential function  $\varphi_2$ , but rewritten down in co-ordinate system No 1, describing the liquid motion generated by No 2 plate vibrations".

2.3. Two parallel boundary problems. Velocity potential function  $\varphi_I$  (or  $\varphi_{II}$ ) has to be a solution of differential equation (3) and this leads to:

$$(9) \quad \Delta\varphi_1 - (1/c^2) \cdot \ddot{\varphi}_1 = 0, \quad \Delta\varphi_2 - (1/c^2) \cdot \ddot{\varphi}_2 = 0.$$

Boundary conditions (4) transform themselves into:

$$(10) \quad \begin{array}{ll} y_1 = 0 & (\partial\varphi_1/\partial y_1) = \dot{w}_1, \quad \partial\varphi_{2(2 \rightarrow 1)}/\partial y_1 = 0; \\ y_2 = 0 & \partial\varphi_{1(1 \rightarrow 2)}/\partial y_2 = 0, \quad (\partial\varphi_2/\partial y_2) = \dot{w}_2. \end{array}$$

2.4. Integrals of Eqs. (9). The integrals of Eqs. (9), satisfying conditions (10) are obtained into forms:

$$(11) \quad \begin{array}{l} \varphi_1 = - \sum_m A_m \cos(m\pi x/h) \cos[k_{2m}(L-y_1)] \sigma \sin(\sigma t) \\ \varphi_2 = - \sum_m B_m \cos(m x/h) \cos[k_{2m}(L+y_2)] \sigma \sin(\sigma t) \end{array}$$

where  $\sigma$  is generally said any circular frequency providing by its special values  $\sigma = \omega_1, \sigma = \omega_2, \sigma = \omega_3, \dots$  the natural frequencies spectrum of the hydroelastic system;  $k_{2m}$  is wave number which has to be determined from the dispersion equation

$$(12) \quad k_{2m}^2 = (\sigma/c)^2 - (m\pi/h)^2.$$

Constants  $A_m$  &  $B_m$  are unknown on the present stage...

2.5. Displacement functions  $w_1$  &  $w_2$ . Let the initial separations

$$(13) \quad w_1(x,t) = W_1(x) \cos(\sigma t), \quad w_2(x,t) = W_2(x) \cos(\sigma t)$$

are introduced. Then, both Eqs. (1) will become

$$(14) \quad \begin{aligned} W_1^{IV} - \Omega_1^2 W_1 &= \sum_m S_1 [A_m \cos(k_{2m} L) + B_m] \cos(m\pi x/h), \\ W_2^{IV} - \Omega_2^2 W_2 &= -\sum_m S_2 [A_m + B_m \cos(k_{2m} L)] \cos(m\pi x/h), \end{aligned}$$

where

$$(15) \quad \Omega_j^4 = [\bar{m}_j \sigma^2 / (EI)_j], \quad S_j = [\rho \sigma^2 / (EI)_j], \quad j = 1, 2,$$

and

$$(16) \quad W_1 = W_1'' = 0, \quad W_2 = W_2'' = 0 \text{ at } x = 0, h.$$

Following the classical procedure one can obtain the integrals of (14) in the forms:

$$(17) \quad \begin{aligned} W_1 &= W_1^0(\Omega_1 x) + \sum_m (S_1 / q_{1m}) [A_m \cos(k_{2m} L) + B_m] \cos(m\pi x/h), \\ W_2 &= W_2^0(\Omega_2 x) - \sum_m (S_2 / q_{2m}) [A_m + B_m \cos(k_{2m} L)] \cos(m\pi x/h), \end{aligned}$$

where

$$(18) \quad \begin{aligned} W_1^0(\Omega_1 x) &= C_1^{(1)} \cos(\Omega_1 x) + C_2^{(1)} \sin(\Omega_1 x) + C_3^{(1)} \operatorname{ch}(\Omega_1 x) + C_4^{(1)} \operatorname{sh}(\Omega_1 x), \\ W_2^0(\Omega_2 x) &= C_1^{(2)} \cos(\Omega_2 x) + C_2^{(2)} \sin(\Omega_2 x) + C_3^{(2)} \operatorname{ch}(\Omega_2 x) + C_4^{(2)} \operatorname{sh}(\Omega_2 x). \end{aligned}$$

Satisfying boundary conditions (10) one can obtain the system

$$(19) \quad \begin{aligned} \sum_m A_m [k_{2m} \sin(k_{2m} L) - \frac{S_1}{q_{1m}} \cos(k_{2m} L)] - B_m \frac{S_1}{q_{1m}} \cos \frac{m\pi x}{h} &= W_1^0(\Omega_1 x), \\ \sum_m A_m \frac{S_2}{q_{2m}} - B_m [k_{2m} \sin(k_{2m} L) - \frac{S_2}{q_{2m}} \cos(k_{2m} L)] \cos \frac{m\pi x}{h} &= W_2^0(\Omega_2 x) \end{aligned}$$

from which the constants  $A_m$  &  $B_m$  can be determined. Putting them into Eqs. (17)

the modes sought can be represented into the forms:

$$(20) \quad \begin{aligned} W_1 &= C_1^{(1)} \sum_m a_{1m} [1 - Q_m^{(11)}] \cos \frac{m\pi x}{h} + C_1^{(2)} \sum_m b_{1m} Q_m^{(21)} \cos \frac{m\pi x}{h} + \\ &+ C_2^{(1)} \sum_m a_{2m} [1 - Q_m^{(11)}] \cos \frac{m\pi x}{h} + C_2^{(2)} \sum_m b_{2m} Q_m^{(21)} \cos \frac{m\pi x}{h} + \\ &+ C_3^{(1)} \sum_m a_{3m} [1 - Q_m^{(11)}] \cos \frac{m\pi x}{h} + C_3^{(2)} \sum_m b_{3m} Q_m^{(21)} \cos \frac{m\pi x}{h} + \\ &+ C_4^{(1)} \sum_m a_{4m} [1 - Q_m^{(11)}] \cos \frac{m\pi x}{h} + C_4^{(2)} \sum_m b_{4m} Q_m^{(21)} \cos \frac{m\pi x}{h}, \end{aligned}$$

where (i) only constants  $C_j^{(1)}$  &  $C_j^{(2)}$ ,  $j = 1, 2, 3, 4$  are unknown; (ii)  $a_{jm}$  &  $b_{jm}$  are obtained from

$$\int_0^h W_1(\Omega_1 x) \cos(m\pi x/h) dx \quad \& \quad \int_0^h W_2(\Omega_2 x) \cos(m\pi x/h) dx$$

see below; second form will be

$$\begin{aligned}
 (21) \quad W_2 = & C_1^{(2)} \sum_m b_{1m} [1 - Q_m^{(22)}] \cos \frac{m\pi x}{h} + C_1^{(1)} \sum_m a_{1m} Q_m^{(12)} \cos \frac{m\pi x}{h} + \\
 & + C_2^{(2)} \sum_m b_{2m} [1 - Q_m^{(22)}] \cos \frac{m\pi x}{h} + C_2^{(1)} \sum_m a_{2m} Q_m^{(12)} \cos \frac{m\pi x}{h} + \\
 & + C_3^{(2)} \sum_m b_{3m} [1 - Q_m^{(22)}] \cos \frac{m\pi x}{h} + C_3^{(1)} \sum_m a_{3m} Q_m^{(12)} \cos \frac{m\pi x}{h} + \\
 & + C_4^{(2)} \sum_m b_{4m} [1 - Q_m^{(22)}] \cos \frac{m\pi x}{h} + C_4^{(1)} \sum_m a_{4m} Q_m^{(12)} \cos \frac{m\pi x}{h} ,
 \end{aligned}$$

where:

$$\begin{aligned}
 (22) \quad a_{1m} &= \int_0^h \cos(\Omega_1 x) \cos \frac{m\pi x}{h} dx, & b_{1m} &= \int_0^h \cos(\Omega_2 x) \cos \frac{m\pi x}{h} dx, \\
 a_{2m} &= \int_0^h \sin(\Omega_1 x) \cos \frac{m\pi x}{h} dx, & b_{2m} &= \int_0^h \cos(\Omega_2 x) \cos \frac{m\pi x}{h} dx, \\
 a_{3m} &= \int_0^h \operatorname{ch}(\Omega_1 x) \cos \frac{m\pi x}{h} dx, & b_{3m} &= \int_0^h \operatorname{ch}(\Omega_2 x) \cos \frac{m\pi x}{h} dx, \\
 a_{4m} &= \int_0^h \operatorname{sh}(\Omega_1 x) \cos \frac{m\pi x}{h} dx, & b_{4m} &= \int_0^h \operatorname{sh}(\Omega_2 x) \cos \frac{m\pi x}{h} dx,
 \end{aligned}$$

and additionally:

$$\begin{aligned}
 (23) \quad Q_m^{(11)} &= d_m^{-1} S_1 [k_{2m} q_{2m} \cos(k_{2m} L) + S_2 \sin(k_{2m} L)] (2/h), \\
 Q_m^{(22)} &= d_m^{-1} S_2 [k_{2m} q_{1m} \cos(k_{2m} L) + S_1 \sin(k_{2m} L)] (2/h), \\
 Q_m^{(21)} &= d_m^{-1} S_1 k_{2m} q_{2m} (2/h), & d_m^{-1} &= (1/d_m), \\
 Q_m^{(12)} &= d_m^{-1} S_2 k_{2m} q_{1m} (2/h)
 \end{aligned}$$

$$(24) \quad d_m = (S_1 q_{2m} + S_2 q_{1m}) \cdot k_{2m} \cos(k_{2m} L) + S_1 S_2 \sin(k_{2m} L).$$

2.6. Natural frequencies spectrum. Together with the integration constants in Eqs. (20) & (21) one parameter only (namely) wave number  $k_{2m}$  is unknown. If one determines it, e.g.

$$(25) \quad (k_{2m} L) = k_{2mn}^*, \quad n = 1, 2, 3, \dots, \infty \Rightarrow k_{2mn} = (k_{2mn}^* / L),$$

then from Eq. (12)

$$(26) \quad \omega_{mn} = +c\sqrt{(m\pi/h)^2 + (k_{2mn}^*/L)^2} \equiv \sigma_{mn}, \quad m < m^*,$$

where  $m^*$  is a number of the members remained in (20) & (21).

Well, satisfying boundary conditions (16) and following the habitual procedure is easy to obtain the main determinant with  $8 \times 8$  elements constructed from the coefficients in front of unknown integration constants  $C_j^{(1)}, \dots, C_j^{(2)}$ , ( $j = 1, 2, 3, 4$ ) and to equate it to zero:

$$(27) \quad \Delta_m [\sigma, k_{2m}, \Omega_1, \Omega_2, S_1, S_2, q_{1m}, q_{2m}, (m\pi/h)] = 0.$$

This will be the equation providing unknown wave numbers  $k_{2mn}$  and the natural frequencies sought.

2.7. Vibration modes. Following the prescription of modal analysis and eigen values problems, the obtained  $k_{2mn}$  &  $\omega_{mn}$  must be put into (20) & (21). All

constants  $C_{jn}^{(1)}$ ,  $C_{jn}^{(2)}$  except one only [e.g.  $C_{1n}^{(1)}$ ] will be determined by the ratios

$$(28) \quad \beta_{jn}^{(1)} = C_{jn}^{(1)} / C_{1n}^{(1)}, \quad \beta_{jn}^{(2)} = C_{jn}^{(2)} / C_{1n}^{(1)}.$$

The last constant (namely  $C_{1n}^{(1)}$ ) must be determined from any norming condition taking into account that the forms  $W_n^{(1)}$  &  $W_n^{(2)}$  are not mutually orthogonal, [Kito, 1970].

### 3. ANALYSIS

3.1. Liquid link. The liquid is playing role of additional link between both structural components vibrating. That is why the vibration modes of every plate are linear sum of the vibration modes of both plates.

3.2. Structural components interaction through the liquid can be find in Ref.[5] (Sheinin, 1967) but in pure shape the idea is refined by Dzhupanov (1974).

3.3. Symetry principle. If one want to separate the mutual influence of the plates due to the liquid, he will see that

$$\bar{Q}_m^{(21)} = d_m^{-1} k_{2m} q_{1m} q_{2m} = \bar{Q}_m^{(12)}.$$

This expresses the Symmetry hydroacoustical principle (Shenderov, 1972). The symmetry of interaction matrices is considered in the fundamental work of Chen & Wambsgans (1972) and investigated in details, afterwards, e.g. in the article of Golovkina, Dzhupanov & Yanatchkov (1984).

3.4. Inertia & Damping. It is interesting to be marked that the influence of the "own" interaction of the each plate with the liquid diminishes the amplitudes of the vibration modes having the reciprocal influence of the oposite plate (which increases the same amplitudes).

3.5. On the natural frequencies spectrum. Obviously equating to zero the quantity expressed by Eq. (24) one can obtain another spectrum of natural frequences. If any of the natural frequences determined by (27) & (26) coincides with any of aforementioned natural frequences in the liquid will occure a disordered jam of chaotic modes but the vibrational modes of the plates will not become infinite.

### 4. REFERENCES

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