

Crack Opening Behavior of Penetrated Crack under Cyclic or Monotonic Loading

Yeon Sik Yoo¹⁾, Seok Hwan Ahn²⁾, Ki Woo Nam²⁾ and Kotijo Ando¹⁾

1) Faculty of Engineering, Yokohama National University, 79-1, Tokiwadai, Hodogayagu, Yokoham, 240, Japan

2) Faculty of Engineering, Pukyong National University, 100, Yongdang-dong, Nam-ku, Pusan, 608-739, Korea

ABSTRACT

Crack opening displacements were examined experimentally at room temperature for both plate and pipe specimen containing a surface crack. Application of crack opening displacement solutions from plate specimens, as proposed by the present authors, to pipe specimens were investigated. Crack opening displacement after penetration could be satisfactorily determined regardless of a type of load using the COD solutions proposed by the authors.

INTRODUCTION

The Leak Before Break (LBB) design philosophy used for high-pressure vessels and energy-related engineering plant equipment has recently been attracting much interest from a safety and economic point of view. The LBB concept is a design philosophy to guarantee that unstable fracture does not occur before a crack penetrates the wall thickness and even after complete penetration for a certain period. Moreover, it is judged that the acceptable LBB case can be made if the leakage is detectable before the crack length reaches a critical length. Studies on unstable fracture due to a crack and the evaluation of the crack opening displacement or crack opening area for leakage inspection of a structure under a monotonic and a cyclic load have been performed for various aspects. The most important steps which should be investigated in a LBB design can be summarized as follows [1]: (a) Throughout the life, a crack should not occur. (b) If a crack occurs, the crack propagation should be small and should be detectable in order to be repaired during regular inspection. (c) If a crack occurs and penetrates the structural parts, the crack propagation and the leakage should be as small as possible. Studies of LBB designs have been performed on various aspects of steps (a) and (b) above. There have also been some studies on step (c) and some useful knowledge about the effects of surface cracks has been reported. The present authors have reported [2] an investigation on the LBB condition and the crack opening behavior under a high fatigue stress. Studies on the crack opening displacement after penetration in a plate and pipe, however, are relatively rare.

The aim of the present study is to investigate the basic behaviors of crack opening displacement (COD) after crack penetration in a plate and a pipe. Basically, three main tasks have been identified. Task 1 was dealt with COD at a plate specimen with surface crack under cyclic loads and Task 2 considers COD when there is an inner and outer surface crack at a pipe specimen under cyclic loads. Task 3 is aimed to evaluate COD of ductile tearing.

CRACK OPENING DISPLACEMENT OF PENETRATED FATIGUE CRACK

Plate subjected to cyclic tensile stress

In order to accurately estimate the characteristics of leak before break under cyclic load, it is a very important to evaluate precisely the crack growth and penetration behavior. The photographs of fatigue fracture surfaces obtained from the plate specimens of 3%NiCrMo steel with surface crack are shown in Fig.1[1-3]. Fig.1(a) shows the result from the small plate specimen under combined tensile and bending stress with a 80 mm width and 10 mm thickness. Fig.1(b) and (c) the results obtained from the stress concentration specimens with a 80 mm width and 10 mm thickness. From these figures, it can be seen that the fatigue crack shapes have almost semicircular.

Stress intensity factor is very important parameter for evaluation the crack growth and penetration behaviors under cycle load in the case of plate with a surface crack. Newman-Raju's formula has been generally applied to analyze the stress intensity factor before crack penetration. The stress intensity factors K_S^e and K_B^e at points S and B (see Fig.2) after penetration, as proposed by the present authors[2], are

$$K_S^e = \delta(a_s)/\delta(a_s) \sigma (\pi a_s)^{0.5} F(\eta_s) \quad (1)$$

$$K_B^e = \delta(a_b)/\delta(a_b) \sigma (\pi a_b)^{0.5} F(\eta_b) \quad (2)$$

where a_s and a_b are the crack length at the front surface and the back surface, respectively, and $a_e = 0.5(3a_s^2 + a_b^2)^{0.5}$, $\eta_s = a_s/W$, $\eta_b = a_b/W$, and

$$F(\eta) = (1 - 0.5\eta + 0.37\eta^2 - 0.044\eta^3) / \{1 - \eta\}^{0.5} \quad (3)$$

The terms $\delta(a)$ in the equations indicate the crack opening displacements and are expressed in the form

$$\delta(a) = 4\sigma a(1 - \nu^2) / EV(\eta) \quad (4)$$

where ν is Poisson's ratio, E is Young's modulus, and

$$V(\eta) = -0.071 - 0.535\eta + 0.169\eta^2 + 0.020\eta^3 - 1.071(1/\eta)\log(1-\eta) \quad (5)$$

When deriving Eqs. (1) and (2), three assumptions were made[2]:

1) The crack after penetration is assumed to retain its semi-elliptical shape, and a_s is assumed to be the major axis of the ellipse. The crack length a_e at the center of the plate thickness can, therefore, be expressed as

$$a_e = 0.5(3a_s^2 + a_b^2)^{0.5} \quad (6)$$

2) The crack opening displacement in the center of the crack after penetration (on the line XX' in Fig.2(a)) is assumed to be the same on the front surface and the back surface.

3) The crack opening displacement $\delta(a_e)$ at the center of the plate thickness of Fig.2(b) is assumed to be the same as the crack opening displacement at the center of a two-dimensional through crack with crack length $2a_e$ in a plate with width $2W$. Hence $\delta(a_e)$ can be expressed as

$$\delta(a_e) = 4\sigma a_e(1 - \nu^2) / EV(\eta) \quad (7)$$

The validity of the above three assumptions was examined via experimental results.

The crack opening displacement after penetration was measured on the front and back surfaces of the plate. This measurement was taken between center points of plate Y mm away from the crack. The distance Y for the small specimens and large specimens were 10mm and 13mm, respectively. The measured value of crack opening displacement is referred to as Δ_{10} and Δ_{13} hereafter. Values of Δ_Y for a two-dimensional through crack with length $2a$ in a plate of width $2W$, is given by the following formula.

$$\Delta_Y = (2\sigma Y/E)[(\pi a/2W)/(\sin(\pi a/2W))]^{(1/2)}[(4W/\pi Y)\cosh^{(-1)}(\cosh(\pi Y/2W) / \cos(\pi a/2W)) - (1+\nu)/(1+(\sin(\pi a/2W)/\sinh(\pi Y/2W))^2)^{(1/2)} + \nu] \quad (8)$$

Eq. (4) is equivalent to Eq. (8) when Y equals 0.

Figure 3 shows a comparison between the experimental values and the calculated values (solid lines) by Eq. (8). In Fig. 3 curve ① represents the $\Delta_{13}/\Delta\sigma$ value obtained from a large specimen[1] under cyclic tension and curve ② indicates the Δ_{10}/σ value obtained from a small specimen[2] under cyclic tension. Curve ③ indicates the $\Delta_{13}/\Delta\sigma$ value obtained from a specimen[3] under combined cyclic tension and bending. It appears that there is good agreement between the measured and the calculated values. It can be suggested, therefore, that the crack opening displacements are correctly evaluated by Eq. (4). Strictly speaking, however, in the range of $a_e/W < 0.35$, the Δ_{13} value on the back surface of the large specimen may be smaller than the calculated value. Based on these results, it can be suggested that crack opening displacement $\delta(a_e)$ at the center of the plate thickness are valid for all cases except for the case where a_e is very small. This fact indicates that the crack opening area and the leakage after penetration can be evaluated by Eq. (4) when the fatigue stress is smaller than the yield stress. When the fatigue stress is large than the yield stress, however, it is not acceptable to use Eq. (4) to evaluate the crack opening area and the leakage after penetration. For this case, another equation proposed by the present authors[4] can be used effectively.

Pipe subjected to cyclic bending moment

The photographs of the fatigue surfaces obtained from the pipe specimens with an outer or inner surface crack are shown in Fig. 4[5-7]. Fig. 4(a)~(d) show the results obtained from the pipe specimens with an outer surface crack which

are subjected to elastic-plastic bending stress respectively. Fig. 4(e)~(h) show the result obtained from the pipe specimens with an inner surface crack subjected to elastic bending stress. These figures were obtained from STS370 pipe with 51mm radius and 8.1mm or 12.7mm thickness. In case the surface trace of the initial crack is larger than its depth (Fig. 4(a) and (e)) regardless of inner or outer crack, the stress intensity factor at the bottom of the notch is larger than that at the edges of its surface crack (notch side). Therefore, the crack initiates first at the bottom of the notch and propagates more rapidly than its surface crack (notch side). The surface crack initiates and propagates afterwards, and eventually the crack penetrates the bottom surface of the pipe. The surface crack with small initial notch (Fig. 4(b)~(d) and (f)~(h)) propagates to the surface trace (notch side) and the depth at the same time, and penetrates the thickness of the pipe.

Evaluation of stress intensity factor before crack penetration ; In order to evaluate the stress intensity factor before penetration of pipe with an outer or inner surface crack, it is necessary for a pipe section to be transformed into a plate. In the plate model, following assumptions were made : plate width(2W) corresponds to the outer perimeter of pipe ($2\pi R_s$), plate thickness is equal to pipe thickness(t). In the case of outer surface crack, crack depth is b , surface crack length is $2C_{s0}$ and the plate was subjected to a tensile stress component equal to actual bending stress (σ_B). In the case of inner surface crack, crack depth is b , surface crack length is $2C_{b0}$ and the plate was subjected to a tensile and bending stress component obtained from actual bending stress (σ_B)

Evaluation of stress intensity factor after crack penetration ; In order to evaluate crack growth behaviors after crack penetration, following pipe model was considered. On the basis of this pipe model, four assumptions were made for deriving the stress intensity factor.

1) The crack opening displacement at the center of the crack after penetration (on the line XX' in Fig. 5) is assumed to be the same on the outer surface and inner surface.

2) After crack penetration, a crack is located symmetrically around the maximum tension point, stress is calculated elastically and one half of the crack angle, θ_M , on the midsection is given by the following equation.

$$\theta_M = (\theta_s + \theta_b) / 2 \quad (9)$$

3) The crack opening displacement $\delta(\theta_M)$ at the center of the wall thickness (on the line XX' in Fig. 5) is assumed to be the same as the crack opening displacement at the center of a simple through wall crack with a crack angle $2\theta_M$ in a pipe. Hence, $\delta(\theta_M)$ can be expressed as the Zahoor's equation.

$$\delta(\theta_M) = 4\sigma_B \cdot \{R_s - (t/2)\} \theta_M \cdot V_b / E \quad (10)$$

$$\text{where, } V_b = 1 + A \{6.071(\theta_M/\pi)^{1.5} + 24.15(\theta_M/\pi)^{2.94}\}$$

$$A = [0.125 \{ (R_s - (t/2)) / t \} - 0.25]^{0.25}$$

$$(\text{valid range : } 5 \leq \{R_s - (t/2)\} / t \leq 10)$$

4) The stress intensity factors K_S and K_B at points S and B (see Fig. 5) after crack penetration are assumed to be equal to the stress intensity factors in simple through wall cracks with a crack angle $2\theta_s$ or $2\theta_b$ respectively, of which the crack opening displacements at the center are exposed to the elastic bending stress corresponding to $\delta(\theta_M)$.

These four assumptions make it possible to express the stress intensity factors for a complex through wall crack such as points S and B in Fig. 5 by using the K formula for a simple through wall crack.

In the case of pipe with an outer surface crack,

$$K_S = K(\theta_s) = \delta(\theta_M) / \delta(\theta_s) \cdot \sigma_B \cdot [\pi \{R_s - (t/2)\} \theta_s]^{0.5} \cdot F_b(\theta_s) \quad (11)$$

$$K_B = K(\theta_b) = \delta(\theta_M) / \delta(\theta_b) \cdot \sigma_B \cdot [\pi \{R_s - (t/2)\} \theta_b]^{0.5} \cdot F_b(\theta_b) \quad (12)$$

In the case of pipe with an inner surface crack,

$$K_S = K(\theta_s) = \delta(\theta_M) / \delta(\theta_s) \cdot \sigma_B \cdot [\pi \cdot R_s \cdot \theta_s]^{0.5} \cdot F_b(\theta_s) \quad (13)$$

$$K_B = K(\theta_b) = \delta(\theta_M) / \delta(\theta_b) \cdot \sigma_B \cdot [\pi \cdot (R_s - t) \cdot \theta_b]^{0.5} \cdot F_b(\theta_b) \quad (14)$$

$$\text{Where, } F_b(\theta_s) = 1+A\{4.5967(\theta_s/\pi)^{1.5} + 2.6422(\theta_s/\pi)^{4.24}\}$$

$$F_b(\theta_b) = 1+A\{4.5967(\theta_b/\pi)^{1.5} + 2.6422(\theta_b/\pi)^{4.24}\}$$

$\delta(\theta_s)$ or $\delta(\theta_b)$ can be introduced by substituting θ_s or θ_b for θ_M in Eq. (10), and $V_b(\theta_s)$ or $V_b(\theta_b)$ can be introduced by substituting θ_s or θ_b for θ_M in Eq. (11)

Crack opening displacements were measured by a clip gauge at maximum tensile stress point and calculated by Eq.(10). Fig. 6 shows a comparison between the experimental crack opening displacements per load ($\delta(\theta_M)/P$) as function of one half of the midsection crack angle (θ_M) and the calculated ones. Although a little scattering is presented in experimental data before θ_b becomes to be equal to θ_s , a quite good agreement between the experimental and the calculated ones is generally represented regardless of initial crack location, bending stress level and crack length at crack penetration.

CRACK OPENING DISPLACEMENT OF PENETRATED DUCTILE CRACK

The LBB definition under monotonic load proposed by Heald et al can be represented by Fig. 7. In the schematic illustrations of load-displacement curve for pipe containing flaws, if the load at break is higher than one at leak, LBB behavior comes into existence. On the contrary, if the load at break is lower than the one at leak, that belongs to NO LBB behavior.

Tada-Paris's equation based on LEFM(Linear Elastic Fracture Mechanics) is well known for a evaluation method of COD about a fully through-wall cracked pipe. The COD when a pipe with a circumferentially fully through-wall crack is subjected to a bending moment is as follows:

$$S_b = \sigma_b/E \cdot (\pi R^2) \cdot I_b(\theta) \quad (15)$$

Where, σ_b is a bending stress, E is Young's modulus and R is a mean radius of pipe. Moreover, $I_b(\theta)$ is as follows:

$$I_b(\theta) = 2\theta^2 \{1 + (\theta/\pi)^{3/2} [8.2 - 12.7(\theta/\pi) + 19.3(\theta/\pi)^2] + (\theta/\pi)^3 [20.4 - 68(\theta/\pi) + 165.2(\theta/\pi)^2 - 187.2(\theta/\pi)^3 + 146.7(\theta/\pi)^4]\} \quad (16)$$

$$(0 < \theta < 100^\circ)$$

Where, θ is a half of crack angle. If a bending stress is higher than yield stress and the effect of plastic region in crack tip should be taken into account, the following θ_{ef} is recommended in place of θ from the above Eq. (16) :

$$\theta_{ef} = \theta + K^2 / (2\pi R \sigma_y^2) \quad (17)$$

Where, σ_y denotes yield stress and K is stress intensity factor.

The elastic COD related to a crack, which penetrates under a loading, could be evaluated by Tada-Paris's method. And the entire COD (the elastic COD + the plastic COD) could not evaluated by using Eq. (17), which takes the effect of a plastic region at the crack tip into account. The main reasons can be considered as follows: (1) Tada-Paris's method is based on LEFM. But in case that a crack penetrated the wall thickness during a loading, the stress was over the yielding point, the correction value by Eq. (17) was in excess of the limit of application as a result of that. (2) A sufficient work-hardening occurred in the ductile materials such as a pipe for nuclear power plant. For the reason, it is considered that the calculated data which was evaluated by the yield stress from Eq. (17) were greater than the real experimental ones.

From the above ones, when a crack penetrated the wall thickness during a loading, it is concluded that the entire COD evaluated by Tada-Paris's method is greater than the real experimental one. That is to say, it is suggested that Tada-Paris's method give a conservative solution in a basis of jet-force and a non-conservative one in a basis of leak inspection. From the above results, it is necessary for investigating another method to evaluate COD when a crack penetrated the wall thickness during a loading. But, it is actually difficult to assume that there is a fully through-wall crack at normal operating. Thus, an approach to consider that a non-penetrating crack penetrates during a loading in pipe is thought to be a common case. These days, most laboratory evaluation of COD is inferred by considering the specimen halves are rigid and rotate about a hinge point. The following two assumptions were made under the basis of this approach :

- 1) The plastic deformation of a pipe occurs only in the cracked part, at which the plastic rotation angle is defined by ϕ_p and the incremental plastic rotation angle is $\Delta\phi_p$,
- 2) This method can be transferred to the evaluation of COD in pipe under bending moment by assuming the hinge point is consistent with neutral axis as shown in Fig.8

From this consideration, referring to Fig. 8, the following relation can estimate COD or COA when a non-penetrating crack penetrates during a loading:

$$\text{COD, } \delta = 2R(1+\cos\beta) \cdot \sin(\Delta\phi_p/2) \quad (18)$$

$$\text{COA, } S = \pi c \delta / 2 \quad (19)$$

Where, β denotes the angle of neutral axis in pipe under bending load and c is a half of crack length, as to say, $c=\theta R$ can be made.

Eq. (18) was proposed on that propose and the appropriateness was investigated on the statically determinate piping system(SD) and the statically indeterminate piping one(SI) in this study. The comparison between the entire COD from the experiment and the one evaluated by Eq. (18) considering the incremental plastic rotation angle was represented in Fig. 9. It is known from the result of Fig. 9 that the experiments show a good consistence with the evaluated, regardless of the systems. From the above ones, it can be concluded that the COD evaluation model proposed in this study is appropriate for investigating the entire COD when a crack penetrates the wall thickness during a loading.

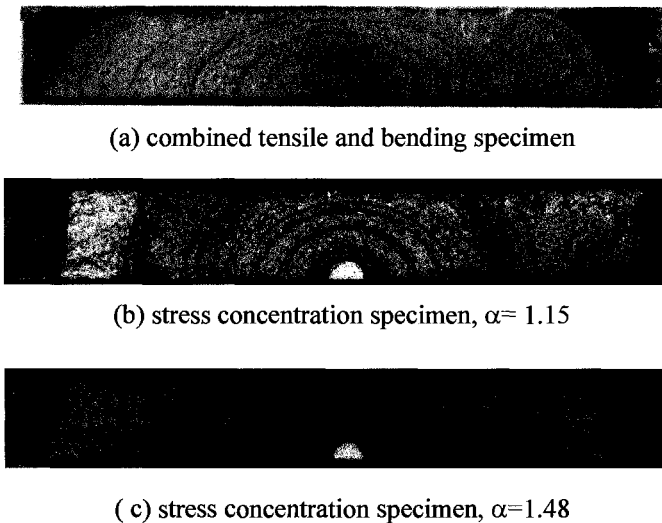


Fig. 1 Photographs of fatigue fracture surface obtained from plate specimen

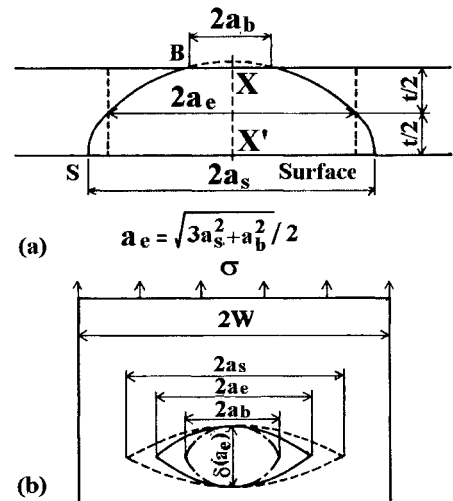


Fig. 2 The crack model used to determine the stress intensity factor after penetration

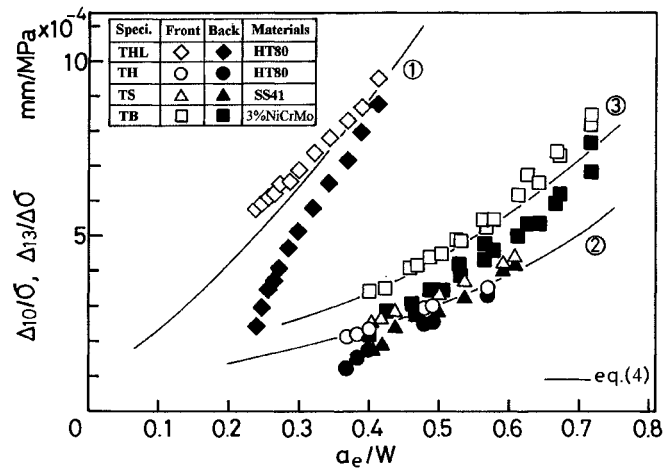
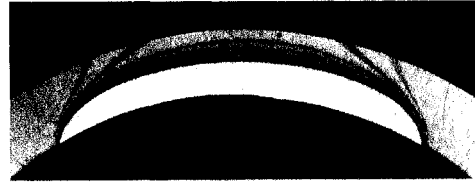


Fig.3 Comparison of experimental with calculated values at the center of the plate of crack opening displacement.



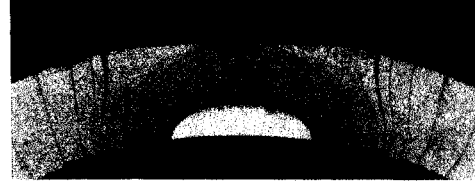
(a) $C_{s0}/t = 2.64$, $\sigma_{max} = 196.0$ MPa, Outer crack



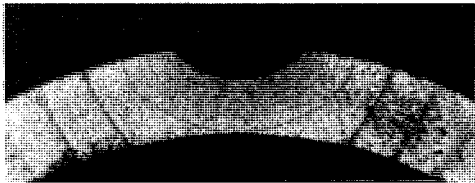
(e) $C_{b0}/t = 2.75$, $\sigma_{max} = 200.0$ MPa, Inner crack



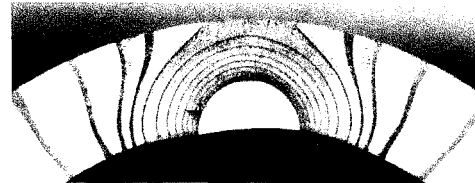
(b) $C_{s0}/t = 0.71$, $\sigma_{max} = 325.9$ MPa, Outer crack



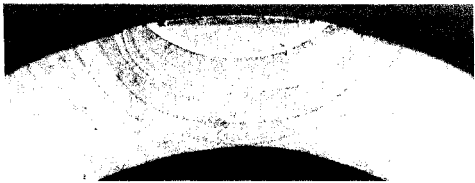
(f) $C_{b0}/t = 0.74$, $\sigma_{max} = 210.0$ MPa, Inner crack



(c) $C_{s0}/t = 0.71$, $\sigma_{max} = 196.0$ MPa, Outer crack



(g) $C_{b0}/t = 0.47$, $\sigma_{max} = 220.0$ MPa, Inner crack



(d) $C_{s0}/t = 0.71$, $\sigma_{max} = 239.6$ MPa, Outer crack



(h) $C_{b0}/t = 0.47$, $\sigma_{max} = 261.0$ MPa, Inner crack

Fig.4 Photographs of fatigue fracture surface

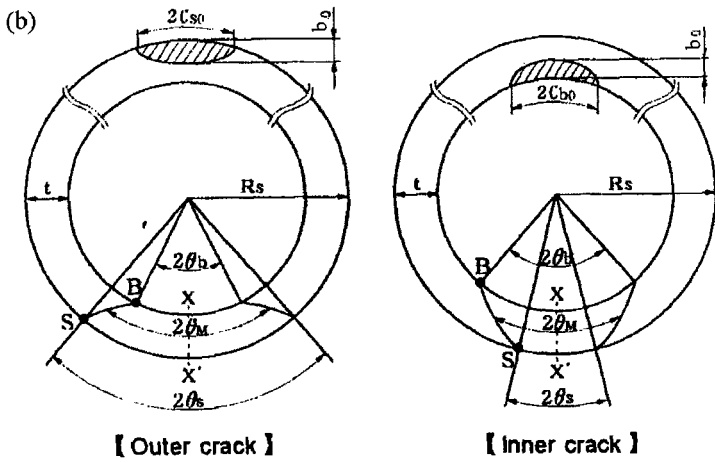


Fig. 5 Model to evaluate the stress intensity factor after crack Penetration

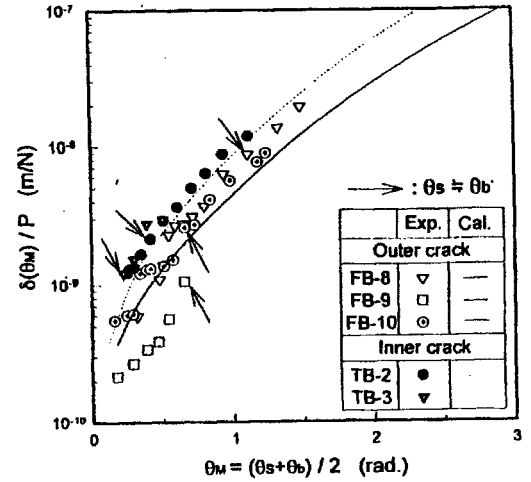


Fig. 6 Comparison between experimental and calculated crack opening displacement

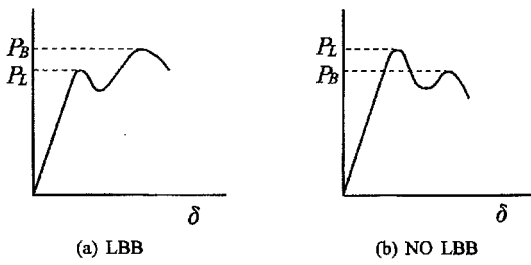


Fig. 7 LBB condition under monotonic load

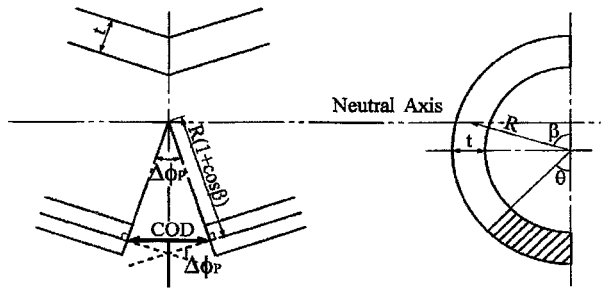


Fig. 8 Model to evaluate COD in pipe under a bending moment

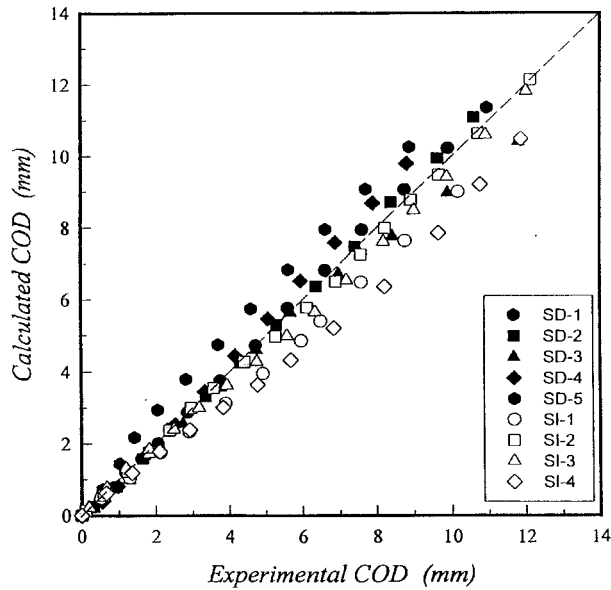


Fig.9 Comparison between calculated and experimental full COD

CONCLUSIONS

The behaviors of crack opening displacement have been studied for plate and pipe specimens with a surface crack. The results obtained from the present study can be summarized as follows:

- (1) The crack opening displacement at the center of the plate thickness was evaluated for all cases regardless of specimen size by using the equation and model proposed by authors.
- (2) After crack penetration, the crack opening displacement was evaluated quantitatively for complex cracks by using the equation and pipe model proposed by authors.
- (3) When a crack penetrated the wall thickness during a loading, the crack opening displacement from a through crack could be evaluated by using the incremental plastic rotation angle.
- (4) This interesting observation warrants further study using various materials to determine its cause and tendency for the penetration behavior of a surface crack, and for possible application in relation to safety and the economics of structures.

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